### AUTOMATIC DIFFERENTIATION IN SOLID MECHANICS INTERPRETATION AND COMPOSITION

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FREE ENERGY FUNCTIONAL AND PDE SOLVERS

$$\psi\left(\boldsymbol{E}\right) = \frac{\lambda}{4} \left(J^2 - 1 - 2\log J\right) - \mu\left(\log J + \operatorname{trace} \boldsymbol{E}\right), \ J = \sqrt{|I_3 + 2\boldsymbol{E}|}$$

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FREE ENERGY FUNCTIONAL AND INVERSE PROBLEMS

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#### Variables to be defined

#### U(1)

U, strain energy density function. For a compressible material, at least one derivative involving J should be nonzero. For an incompressible material, all derivatives involving J will be ignored. The strain invariants— $\bar{I}_1$ ,  $\bar{I}_2$ , and J—are defined in Hyperelastic behavior of rubberlike materials.

#### U(2)

 $\tilde{U}_{dev}$ , the deviatoric part of the strain energy density of the primary material response. This quantity is needed only if the current material definition also includes Mullins effect (see Mullins effect).

UI3(1)

$\partial U / \partial \bar{I}_1.$
UI1(2)

 $\partial U/\partial \bar{I}_2$ .

UI1(3)

$\partial U/\partial J.$
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0,1	- 2 -	( 1 )	,

$\partial^2 U / \partial \bar{I}_1^2$ .	$\partial^3 U / \partial {ar I}_1^2 \partial J.$
UI2(2)	UI3(2)
$\partial^2  U /  \partial  {ar I}_2^{\ 2}.$	$\partial^3  U /  \partial  {ar I}_2^{\ 2}  \partial  J.$
UI2(3)	UI3(3)
$\partial^2 U/\partial J^2.$	$\partial^3 U / \partial \bar{I}_1 \partial \bar{I}_2 \partial J.$
UI2(4)	UI3(4)
$\partial^2 U/\partial {ar I}_1 \partial {ar I}_2.$	$\partial^3  U /  \partial  {ar I}_1  \partial  J^2.$
UI2(5)	UI3(5)
$\partial^2 U / \partial I_1 \partial J.$	$\partial^3  U /  \partial  {ar I}_2  \partial  J^2.$
UI2(6)	UI3(6)
$\partial^2 U / \partial \bar{I}_2 \partial J.$	$\partial^3 U / \partial J^3$ .

# Fully automated commercial package (Solid Mechanics, FEM)

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$\partial^2 U / \partial {I_2}^2.$	$\partial^3  U /  \partial  {ar I}_2^{\ 2}  \partial  J.$
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- Fully automated commercial package (Solid Mechanics, FEM)
- Complex interface (too many inputs)

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|--|--|

$\partial^2 U / \partial \bar{I}_1^2$ .	$\partial^3 U / \partial {ar I}_1^2 \partial J.$
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# Fully automated commercial package (Solid Mechanics, FEM)

- Complex interface (too many inputs)
- ► Unstable for small deformation due to the choice of interface design
   *F* = *I* + ∇<sub>X</sub>*u*

### ABAOUS **UHYPER: USER SUBROUTINE**

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#### UI1(1) 0.77 / 0.7

UI2(2)

UI2(3)

UI2(4)

UI2(5)

UI2(6)

$\partial U / \partial I_1$ .
UI1(2)
$\partial U/\partial {ar I}_2.$
UI1(3)
$\partial U / \partial J.$
UI2(1)
$\partial^2 U / \partial \bar{I}_1^2$

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- Fully automated commercial package (Solid Mechanics, FEM)
- Complex interface (too many inputs)
- ► Unstable for small deformation due to the choice of interface design  $F = I + \nabla_{\mathbf{x}} u$
- Not easy to change the interface

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UI3

a

 $\partial^3$ 

 $\partial^3 U$ 

 $\partial^3 U / \partial \bar{I}_1 \partial J^2$ .

 $\partial^3 U / \partial \bar{I}_2 \partial J^2$ .

 $\partial^3 U / \partial J^3$ .

" J J .

UI3(3)

UI3(4)

UI3(5)

UI3(6)

UI3 (:

#### UI1(1)

 $\partial U/\partial \bar{I}_{1}$ UI1(2)  $\partial U/\partial \bar{I}_{2}$ . UI1(3)  $\partial U / \partial J$ . UI2(1)  $\partial^2 U / \partial \bar{I}_1^2$ . UI2(2) $\partial^2 U / \partial I_2^2$ . UI2(3)  $\partial^2 U / \partial J^2$ . UI2(4)  $\partial^2 U / \partial \bar{I}_1 \partial \bar{I}_2.$ UI2(5)  $\partial^2 U / \partial I_1 \partial J.$ UI2(6)  $\partial^2 U / \partial \bar{I}_2 \partial J.$ 

naterial, at least one derivative involving<br/>Il derivatives involving J will be ignored.<br/>yperelastic behavior of rubberlikecommercial package<br/>(Solid Mechanics, FEM)the primary material response. This<br/>also includes Mullins effect (seeComplex interface<br/>many inputs)AD helps us to create a<br/>more generic interface<br/>more generic interface<br/>(one input function,  $\psi(E)$ ).able for small<br/>mation due to the<br/>of interface design<br/> $= I + \nabla_X u$ 

Fully automated

Not easy to change the interface

# RATEL: EXTENSIBLE, PERFORMANCE-PORTABLE SOLID MECHANICS HTTPS://GITLAB.COM/MICROMORPH/RATEL



### RATEL: EXTENSIBLE, PERFORMANCE-PORTABLE SOLID MECHANICS Composition and Abstraction - LIBCEED: https://libceed.org/en/latest/

### $A = \mathcal{P}^T \mathcal{E}^T B^T D B \mathcal{E} \mathcal{P}$



- Purely algebraic high-order FEM
- Single source Vanilla C for physics
- Various CPU and GPU backends
- Backend plugins with run-time selection ./bps -ceed /gpu/cuda
- Support for Matrix-assembly and Matrix-free
- Operator abstraction
- User choice of data storage at quadrature point

### RATEL: EXTENSIBLE, PERFORMANCE-PORTABLE SOLID MECHANICS Composition and Abstraction - PETSC and Enzyme-AD

# **PETSc:**

https://petsc.org/release/

- Parallel solution of PDEs
- ► CPUs (MPI)
- ► GPUs
  - CUDA
  - HIP
  - OpenCL
- ► Hybrid MPI-GPU
- Optimization (PETSc/Tao)

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# **Enzyme AD:**

https://enzyme.mit.edu/

- High-Performance Automatic Differentiation
- ► Work at the LLVM level
- Support for variety of languages (C/C++, Julia, Rust, Fortran, etc)
- ► *reverse* and *forward* mode AD

### INITIAL VS CURRENT CONFIGURATION



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### RATEL - ENZYME AD INITIAL CONFIGURATION - FORWARD SPLIT

```
// S = d(\psi) / d(E) [Reverse mode]
void SecondPiolaKirchhoffStress_NeoHookean_AD(...) {
    __enzyme_autodiff((void *)StrainEnergy, ...);
```

#### // Call forward S and return tape

```
__enzyme_augmentfwd(
  (void *)SecondPiolaKirchhoffStress_NeoHookean_AD,
  enzyme_allocated, tape_bytes, enzyme_tape, tape,
  enzyme_nofree, ...);
```

```
// Compute dS using the stored tape [Forward-split]
__enzyme_fwdsplit(
  (void *)SecondPiolaKirchhoffStress_NeoHookean_AD,
  enzyme_allocated, tape_bytes, enzyme_tape, tape, ...);
```



# RATEL - ENZYME AD

CURRENT CONFIGURATION - REVERSE AND FORWARD



```
// Compute tau = (dPsi / de) * (2 e + I) [Reverse]
void Kirchhofftau Voigt NeoHookean AD(...) {
  enzyme autodiff((void *)StrainEnergy, ...);
  . . .
  for (int j = 0; j < 6; j++)
    b Voigt[j] = 2 * e Voigt[j] + (j < 3);
  . . .
  RatelMatMatMult(1., dPsi, b, tau);
// Compute dtau [Forward]
CEED OFUNCTION HELPER void dtau fwd(...) {
  ___enzyme_fwddiff(
  (void *) Kirchhofftau Voigt NeoHookean AD, ...);
```

# Ratel - Enzyme AD

PERFORMANCE FOR DIFFERENT JACOBIAN REPRESENTATIONS

Problem	Storage	Scalars	Time (s)
current	$W;  abla_x oldsymbol{\xi}, oldsymbol{ au}, J-1$	17	36.2
initial	$W, \nabla_X \boldsymbol{\xi}; \nabla_X \boldsymbol{u}$	19	48.4
initial-AD	$W,  abla_X oldsymbol{\xi};  abla_X oldsymbol{u}, S,  ext{tape}$	31	53.9
current-AD	$W; \nabla_x \boldsymbol{\xi}, \boldsymbol{e}$	16	55.8

$$\begin{array}{c} \textbf{Current-Analytical} \\ \hline \boldsymbol{\varphi}_{X} \textbf{u} \\ \hline \nabla_{X} \textbf{u} \\ \hline \boldsymbol{\varphi}_{X} \boldsymbol{u} \\ \hline \boldsymbol{\varphi}_{X} \boldsymbol{u} \\ \hline \boldsymbol{\varphi}_{X} \boldsymbol{\delta} \textbf{u} \end{array} \xrightarrow{\boldsymbol{\varphi}_{X} \boldsymbol{\delta}_{X} \boldsymbol{\delta}$$

$$\begin{array}{c} \nabla_{X} \boldsymbol{u} \\ \hline \nabla_{X} \boldsymbol{u} \\ \boldsymbol{\tau} = \frac{\partial \psi}{\partial \boldsymbol{e}} \left( 2\boldsymbol{e} + \boldsymbol{I} \right) \\ \hline \boldsymbol{\tau} = \frac{\partial \psi}{\partial \boldsymbol{e}} \left( 2\boldsymbol{e} + \boldsymbol{I} \right) \\ \hline \boldsymbol{\sigma}_{X} \delta \boldsymbol{u} \\ \hline \boldsymbol{\delta} \boldsymbol{\tau} = \frac{\partial \boldsymbol{\tau}}{\partial \boldsymbol{e}} \end{array}$$

$$\begin{array}{c} \textbf{Current-Analytical} \\ \hline \boldsymbol{\nabla}_{X} \textbf{u} \\ \hline \nabla_{X} \textbf{u} \\ \hline \boldsymbol{\nabla}_{X} \textbf{u} \\ \hline \boldsymbol{\nabla}_{X} \textbf{u} \\ \hline \boldsymbol{\nabla}_{X} \boldsymbol{u} \\ \hline \boldsymbol{\nabla}_{X} \boldsymbol{u} \\ \hline \boldsymbol{\nabla}_{X} \delta \textbf{u} \end{array} \xrightarrow{\boldsymbol{\nabla}_{X} \delta \boldsymbol{u}} \begin{array}{c} \boldsymbol{\nabla}_{X} \boldsymbol{u} \\ \boldsymbol{\nabla}_{X} \delta \boldsymbol{u} \\ \hline \boldsymbol{\nabla}_{X} \delta \boldsymbol{u} \\ \hline \boldsymbol{\nabla}_{X} \delta \boldsymbol{u} \end{array} \xrightarrow{\boldsymbol{\nabla}_{X} \delta \boldsymbol{u}} \begin{array}{c} \boldsymbol{\nabla}_{X} \boldsymbol{\delta} \boldsymbol{u} \\ \boldsymbol{\nabla}_{X} \delta \boldsymbol{u} \\ \hline \boldsymbol{\nabla}_{X} \delta \boldsymbol{u} \\ \hline \boldsymbol{\nabla}_{X} \delta \boldsymbol{u} \end{array} 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$$Current-Analytical \rightarrow Res$$

$$e = e(\nabla_X u)$$

$$J = J(\nabla_X u)$$

$$\tau = \frac{\lambda}{2} (J^2 - 1) I_3 + 2\mu e$$

$$\tau, \nabla_x X, J - 1$$

$$\nabla_X \delta u$$

$$\delta \epsilon = \delta \epsilon (\nabla_x c \qquad \delta \tau$$

$$Jac$$

$$Jac = Jac (\nabla_x \delta u, J, \tau, \delta \epsilon)$$

$$\begin{array}{c} e = e(\nabla_X u) \\ \hline & \bullet \tau = \frac{\partial \psi}{\partial e} \left( 2e + I \right) \\ \hline & \bullet \tau = \frac{\partial \psi}{\partial e} \left( 2e + I \right) \\ \hline & \bullet r = \frac{\partial \psi}{\partial e} \left( 2e + I \right) \\ \hline & \bullet r = \frac{\partial \tau}{\partial e} \end{array}$$

$$\begin{array}{c} \textbf{Current-Analytical} \\ \hline \boldsymbol{\nabla}_{X}\boldsymbol{u} \\ \hline \boldsymbol{\nabla}_{X}\delta\boldsymbol{u} \\ \hline \boldsymbol{\nabla$$





Enzyme-aware clangd

- ► Enzyme-aware clangd
- ► Compile code with -00

- ► Enzyme-aware clangd
- ► Compile code with -00
- Calling Enzyme in a debugger

- ► Enzyme-aware clangd
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$$d(\boldsymbol{A}\boldsymbol{A}^{-1})=d(\boldsymbol{A})\boldsymbol{A}^{-1}+\boldsymbol{A}d(\boldsymbol{A}^{-1})$$

### OUTLOOK Towards Plasticity

